



Benchmark Example No. 34

Ultimate Bearing Capacity of Concrete and Steel under Fire

SOFiSTiK | 2023

VERiFiCATION
BE34 Ultimate Bearing Capacity of Concrete and Steel under Fire

VERiFiCATION Manual, Service Pack 2023-10 Build 44

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SOFiSTiK AG

HQ Nuremberg
Flataustraße 14
90411 Nürnberg
Germany

T +49 (0)911 39901-0
F +49(0)911 397904

Office Garching
Parkring 2
85748 Garching bei München
Germany

T +49 (0)89 315878-0
F +49 (0)89 315878-23

info@sofistik.com
www.sofistik.com

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The manual and the program have been thoroughly checked for errors. However, SOFiSTiK does not claim that either one is completely error free. Errors and omissions are corrected as soon as they are detected.

The user of the program is solely responsible for the applications. We strongly encourage the user to test the correctness of all calculations at least by random sampling.

Front Cover

Volkstheater, Munich Photo: Florian Schreiber

Overview

Element Type(s):	BF2D, SH3D
Analysis Type(s):	STAT, MNL
Procedure(s):	LSTP
Topic(s):	FIRE
Module(s):	TALPA, ASE
Input file(s):	capacity.dat , quad_34.dat

1 Problem Description

This benchmark is concerned with the validation of the structural analysis in case of fire with respect to the general calculation method according to DIN EN 1992-1-2. Therefore test case 6 is employed as presented in Annex CC of the standard DIN EN 1992-1-2/NA:2010-03 [1]. In this example the ultimate bearing capacity of structural steel and concrete in compression, for the model of Fig. 1, at varying temperature levels, is investigated.

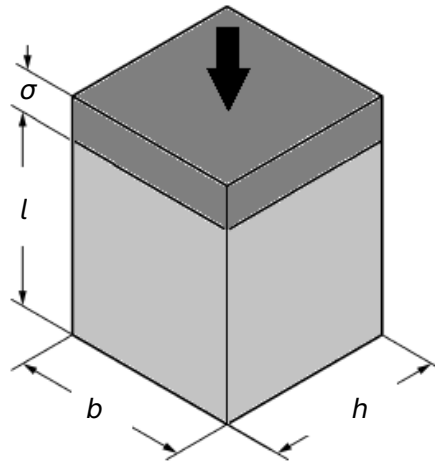


Figure 1: Problem Description

2 Reference Solution

The aim of Annex CC [1] is to check the applicability of the programs for engineering-based fire design on real structures. In this case the influence of the combination of temperature and compressive loading, on the ultimate bearing capacity is examined.

3 Model and Results

The properties of the model are defined in Table 1. A fictional beam as depicted in Fig. 1 is examined here, for the case of structural steel S 355 and of concrete C 20/25, with cross-sectional dimensions $b/h = 10/10 \text{ mm}$, $l = 100 \text{ mm}$ and $b/h = 31.6/31.6 \text{ mm}$, $l = 100 \text{ mm}$, respectively. The boundary conditions are set such that stability failure is ruled out. The analysis is performed with TALPA, where the FIBER beam element is utilised. The computed and the reference results are presented in Table 2 for structural steel and in Table 3 for concrete.

Table 1: Model Properties

Material Properties		Geometric Properties		Test Properties
Steel	Concrete	Steel	Concrete	
S 355	C 20/25	$l = 100 \text{ mm}$	$l = 100 \text{ mm}$	Initial Conditions:
$f_{yk} = 355 \text{ MPa}$	$f_{ck} = 20 \text{ MPa}$	$h = 100 \text{ mm}$	$h = 31.6 \text{ mm}$	$\Theta = 20^\circ\text{C}$
Stress-strain: DIN EN 1993-1-2	Stress-strain: DIN EN 1992-1-2	$b = 10 \text{ mm}$	$b = 31.6 \text{ mm}$	Homog. temp.: 20, 200, 400, 600, 800°C

Table 2: Results for Structural Steel - FIBER beam

Θ [° C]	Ref. [1] $N_{R,fi,k}$ [kN]	SOF. $N_{R,fi,k'}$ [kN]	e [kN]	e_r [%]	Tol.
20	-35.5	-35.5	0.000	0.000	
200	-35.5	-35.5	0.000	0.000	$\pm 3 \%$
400	-35.5	-35.5	0.000	0.000	and
600	-16.7	-16.7	-0.015	0.090	± 0.5 [kN]
800	-3.9	-3.9	0.005	-0.128	

Table 3: Results for Concrete - FIBER beam

Θ [° C]	Ref. [1] $N_{R,fi,k}$ [kN]	SOF. $N_{R,fi,k'}$ [kN]	e [kN]	e_r [%]	Tol.
20	-20.0	-20.0	-0.029	0.144	
200	-19.0	-19.0	-0.027	0.144	$\pm 3 \%$
400	-15.0	-15.0	-0.022	0.144	and
600	-9.0	-9.0	-0.013	0.144	± 0.5 [kN]
800	-3.0	-3.0	-0.004	0.144	

Next step is the analysis of the same example with ASE where the QUAD element is now tested. The results are presented in Table 4 for structural steel and in Table 5 for concrete.

Table 4: Results for Structural Steel - QUAD

Θ [° C]	Ref. [1]	SOF.	e [kN]	e_r [%]	Tol.
	$N_{R,fi,k}$ [kN]	$N_{R,fi,k'}$ [kN]			
20	-35.5	-35.5	0.000	0.000	
200	-35.5	-35.5	0.000	0.000	± 3 %
400	-35.5	-35.5	0.000	0.000	and
600	-16.7	-16.7	-0.015	0.090	± 0.5 [kN]
800	-3.9	-3.9	0.005	-0.128	

Table 5: Results for Concrete - QUAD

Θ [° C]	Ref. [1]	SOF.	e [kN]	e_r [%]	Tol.
	$N_{R,fi,k}$ [kN]	$N_{R,fi,k'}$ [kN]			
20	-20.0	-20.0	-0.029	0.144	
200	-19.0	-19.0	-0.037	0.193	± 3 %
400	-15.0	-15.0	-0.023	0.156	and
600	-9.0	-9.0	-0.013	0.150	± 0.5 [kN]
800	-3.0	-3.0	-0.015	0.489	

4 Conclusion

This example verifies the influence of compressive loading on the ultimate bearing capacity under different temperature levels. It has been shown that the calculation results are in very good agreement with the reference results for both the QUAD layer element and the FIBER beam element.

5 Literature

- [1] *DIN EN 1991-1-2/NA: Eurocode 1: Actions on structures, Part 1-2/NA: Actions on structures exposed to fire*. CEN. 2010.